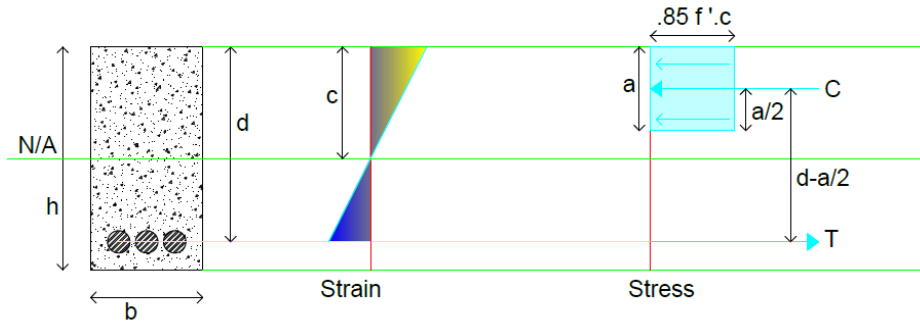


Singly Reinforced Beam Section



Assumptions: Steel only in tension
 Steel Yields before the concrete reaches the maximum compression
 Uses ACI 318 - 08 ; CODE: 10.2.7
 Equivalent Concrete Stress Distribution

Variable Definitions

A_s = Area of Tension Reinforcement (steel)

E = Young's Modulus

A'_s = Area of Compression

ϵ_s = Steel Strain

b = Width of Compression Zone

ϵ_y = Yielding Steel Strain

h = Height

M_n = Nominal Moment

d = Distance from the extreme/top fiber in compression to the centroid of tension steel

ϵ_{cu} = Ultimate Compressive Strain of Concrete

f'_c = Compressive Strength of Concrete

C = Compressive Force

T = Tensile Force

a = Distance from the top fiber in compression to the bottom of the equivalent compressive stress distribution

c = Distance from the top fiber in compression to the neutral axis

β_1 = Constant from the ACI 318 - 08 manual that is used to calculate, c or a

f_y = Yielding Stress of Steel Rebar

Given:

- Geometric structure of the beam

$h := 24\text{-in}$ $b := 14\text{-in}$ $d := 21\text{-in}$

- Properties of Concrete

Compressive Strength of the Concrete $f'_c := 3\text{-ksi}$

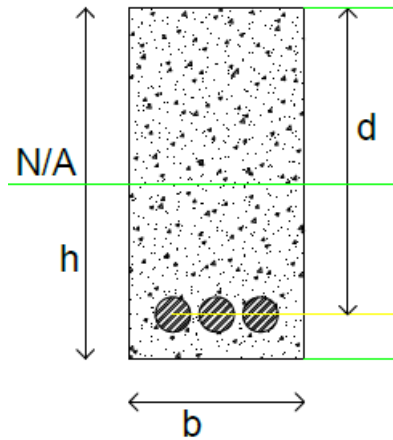
- Properties of Steel

Rebar_{number} := 9 Rebar_{amount} := 3

Rebar_{grade} := 60

Yielding Stress of Steel Rebar $f_y := \text{Rebar}_{\text{grade}} \cdot \text{ksi}$

$f_y = 60\text{ksi}$



Data :=



Area of steel $A_S := (\text{Rebar}_{\text{amount}} \cdot \text{Data})_{\text{match}(\text{Rebar}_{\text{number}}, \text{Data} \langle 0 \rangle)} \cdot 0,2 \text{ in}^2$ $A_S = 3 \cdot \text{in}^2$

Strategy

Step 1: Check that $A_s > A_{smin}$ (code) **NEEDS TO BE BUILT IN ONCE I KNOW THE CODE**

Step 2: Compute "a" based on the assumption that the steel is yielding before the concrete

Step 3: verify that the steel is yielding

Step 4: Calculate the nominal moment " M_n "

Step 2:

Computation of " a "

C is equal to T, and each is just the summation of the forces for the whole object.

$$C = T = .85 \cdot f'_c \cdot a \cdot b = A_s \cdot f_y$$

$$a := \frac{A_s \cdot f_y}{.85 \cdot f'_c \cdot b} \quad \frac{\text{in}^2 \cdot \frac{\text{lbf}}{\text{in}^2}}{\left(\frac{\text{lbf}}{\text{in}^2}\right) \cdot \text{in}} = 1 \text{ in}$$

$$a = 5.04202 \text{ in}$$

Computation of " β_1 "

(ACI 10.2.7.3)

"For f'_c between 2500 and 4000 psi, β_1 shall be taken as 0.85. For f'_c above 4000 psi, β_1 , shall be reduced linearly at a rate of .05 for each 1000 psi of strength in excess of 4000 psi, but β_1 shall not be taken less than 0.65."

$$\beta_1 := \text{if} \left[f'_c \leq 4 \cdot \text{ksi}, 0.85, \max \left[0.85 - .05 \cdot \left(\frac{f'_c - 4 \text{ksi}}{1 \cdot \text{ksi}} \right), 0.65 \right] \right]$$

$$\beta_1 = 0.85$$

Computation of " c "

(ACI 10.2.7.1)

"Concrete stress of $.85 \cdot f'_c$ shall be assumed uniformly distributed over an equivalent compression zone bounded by edges of the cross section and a straight line located parallel to the neutral axis at a distance $a = c \cdot \beta_1$ from the fiber of maximum compressive strain. "

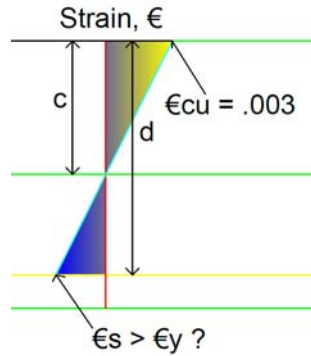
$$c = a / \beta_1$$

$$c := \frac{a}{\beta_1}$$

$$c = 5.93178 \text{ in}$$

Step 3:

The ultimate compressive strain of the concrete is a constant and known to be .0035. By calculating " c " in Step 2, and knowing the value of " d ", we are able to use simple triangular geometry to calculate ϵ_s . We can then check to see if ϵ_s is actually yielding by comparing it to ϵ_y , the yielding strain of the steel that is derived by using the Young's modulus and the yielding stress.



$E = \text{Young's Modulus} = \sigma/\epsilon = \text{stress} / \text{strain}$

*Using the young's modulus assumes elastic behavior and obey hooke's law.

*E is a property of the material and is constant.

$E_{\text{steel}} = 29,000,000 \text{ psi (29,000 ksi)}$

$\epsilon_{\text{cu}} = \text{ultimate compressive strain of concrete} = .0035$

Computation of " ϵ_y "

$E := 29000 \cdot \text{ksi}$

$f_y = 60 \text{ ksi}$

$\epsilon_y = \sigma/E = f_y / E$

Yielding Strain of Steel Rebar

$\epsilon_y := \frac{f_y}{E}$

$\epsilon_y = 0.00207$

Computation of " ϵ_s " and comparison to " ϵ_y "

$\epsilon_{\text{cu}} := .003$

$\epsilon_s := \frac{(d - c) \cdot \epsilon_{\text{cu}}}{c}$

$\epsilon_s = 0.00762$

***If " ϵ_s " is less than " ϵ_y " then reevaluation is required.**

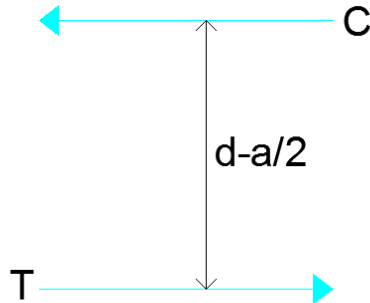
$\epsilon_s = 0.00762$

$\epsilon_y = 0.00207$

$\epsilon_{\text{ten}} := \text{if}(\epsilon_s \geq \epsilon_y, \text{"OK"}, \text{"NG"})$

$\epsilon_{\text{ten}} = \text{"OK"}$

Step 4:



Calculation of the nominal moment is easily computed by multiplying either the compressive force, C, or tension force, T, by the moment arm. Either method is effective.

$$M_n = T (d-a/2)$$

The Tension force can be calculated by Knowing the tensile stress that is applied to the steel. Fundamentally, stress is a force divided by the area the force is applied to. The entire tension force is being applied through the cross sectional area of the steel rebar, which is a known quantity.

$$\sigma = F/A$$

Tensile Stress = Yielding Stress assumed at the beginning of the analysis.

$$f_y = 60 \text{ ksi}$$

The Area of the Steel was calculated previously.

$$A_S = 3 \text{ in}^2$$

$$T := f_y \cdot A_S$$

$$T = 180 \text{ kip}$$

$$M_n := T \cdot \left(d - \frac{a}{2} \right)$$

$$M_n = 1.28421 \times 10^9 \frac{\text{lb} \cdot \text{in}^2}{\text{s}^2}$$